

COMMON STRUCTURAL RULES FOR  
BULK CARRIERS

Stress concentration factor for the hatch corners

## Doubts in the CSR bulk formula ( $K_{gh}$ )

COMMON STRUCTURAL RULES FOR  
BULK CARRIERS

Chapter 8 - Fatigue check of structural details

Section 5 – STRESS ASSESSMENT OF HATCH CORNERS

### 3. Hot spot stress

#### 3.1 Hot spot stress range

##### 3.1.1

The hot spot stress range, in  $N/mm^2$ , is to be obtained from the following formula:

$$\Delta\sigma_W = K_{gh} \cdot \Delta\sigma_{WT}$$

where:

$K_{gh}$  : Stress concentration factor for the hatch corner, taken equal to:

$$K_{gh} = \frac{r_a + 2r_b}{3r_a} \left[ 1 + \left( \frac{b}{1.23\ell_{CD} + 0.8b} \frac{0.22\ell_{CD}}{r_a} \right)^{0.65} \right], \text{ to be taken not less than 1.0}$$

$r_a$  : Radius, in m, in major axis

$r_b$  : Radius, in m, in minor axis ( if the shape of corner is a circular arc,  $r_b$  is to be equal to  $r_a$ )

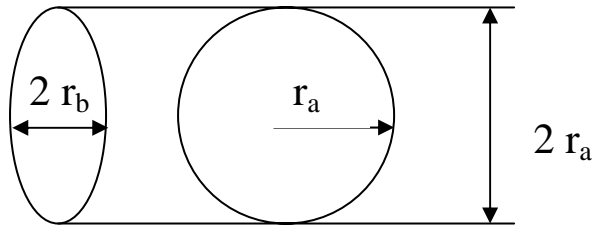
$\ell_{CD}$  : Length of cross deck, in m, in longitudinal direction

$b$  : Distance, in m, from the edge of hatch opening to the ship's side.

## Correction factor for elliptic corners

In the bulk formula,  $r_a$  is used for rounded corners (the radius in major axis) as a basis for elliptic corners. They attribute a correction factor to take into account the influence of elliptic shape.

Here is the equivalence between the two shapes:



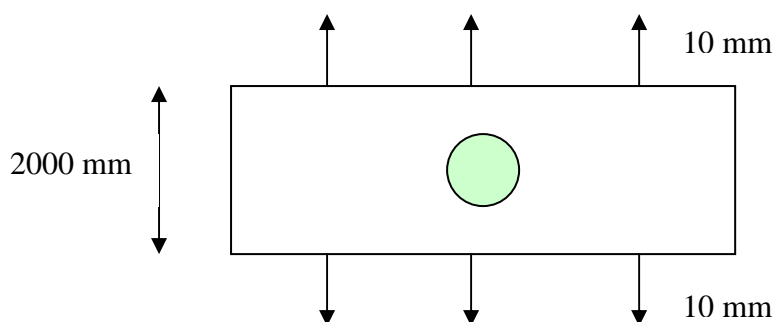
with the following correction factor to apply to get the elliptic stress concentration factor from the rounded one:

$$f_c = \frac{1}{3} + \frac{2r_b}{3r_a}$$

Here follow the original text describing the correction factor:

*This correction factor gives the ratio of stress concentration for the tension of an infinite width thin element with an elliptic hole to that with a circular hole. In this equation,  $r_a$  denotes the radius in major axis and  $r_b$  denotes the radius in minor axis. This correction factor can be applied to the stress concentration factor for the fillet shoulder with circular arc shape of radius  $r_a$ .*

We test the correction factor with ANSYS 9.0 finite element software. We used shell elements of 10 mm thickness. We model plates of 2 by 6 meters with holes in the middle and impose displacements of 20 mm in the small direction as shown in the figure below. We use a 206000 MPa Young modulus and a 0.3 Poisson ratio.

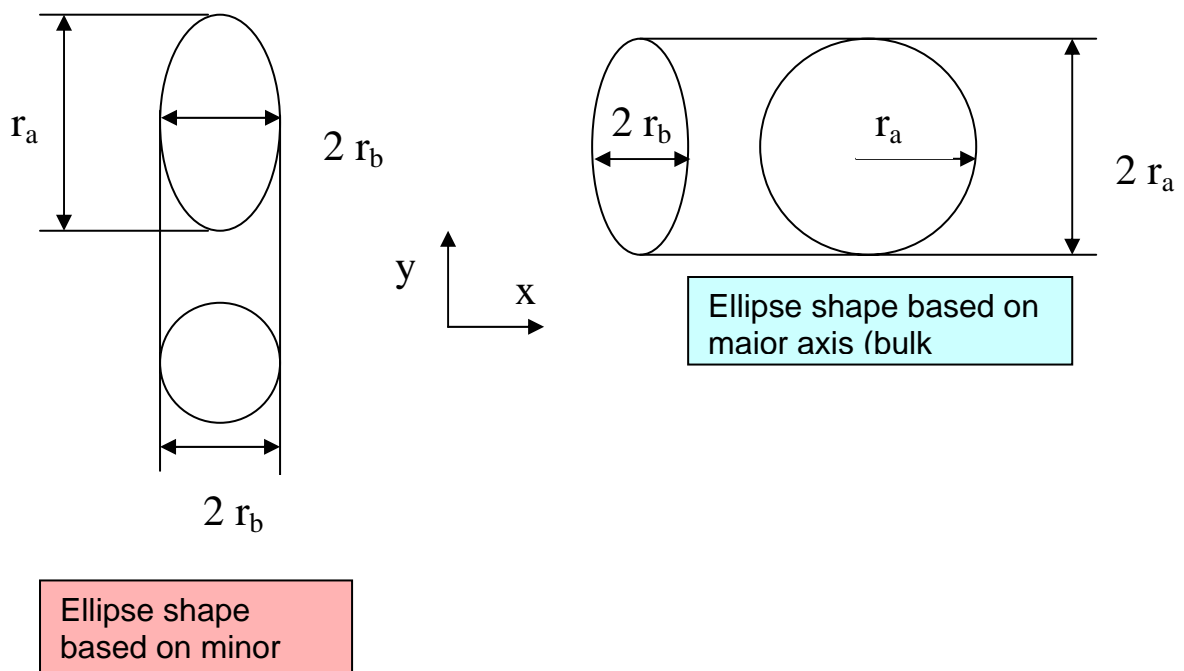


We compare six different shapes to the circular one.

Dimensions of the compared ellipses

Shape	Arm length in x axis	Arm length in y axis
<b>Circular hole</b>	200	200
Ellipse 1	50	200
Ellipse 2	75	200
Ellipse 3	100	200
Ellipse 4	200	250
Ellipse 5	200	300
Ellipse 6	200	400

Ellipse shapes 4, 5 and 6 are other kind of ellipse shape that those used for bulk formula. The reference axis is the minor one.



### Measures

- Mean stress

The mean stress is calculated as follow for a simple tensile test without any hole:

$$\sigma_{mean} = E \varepsilon$$

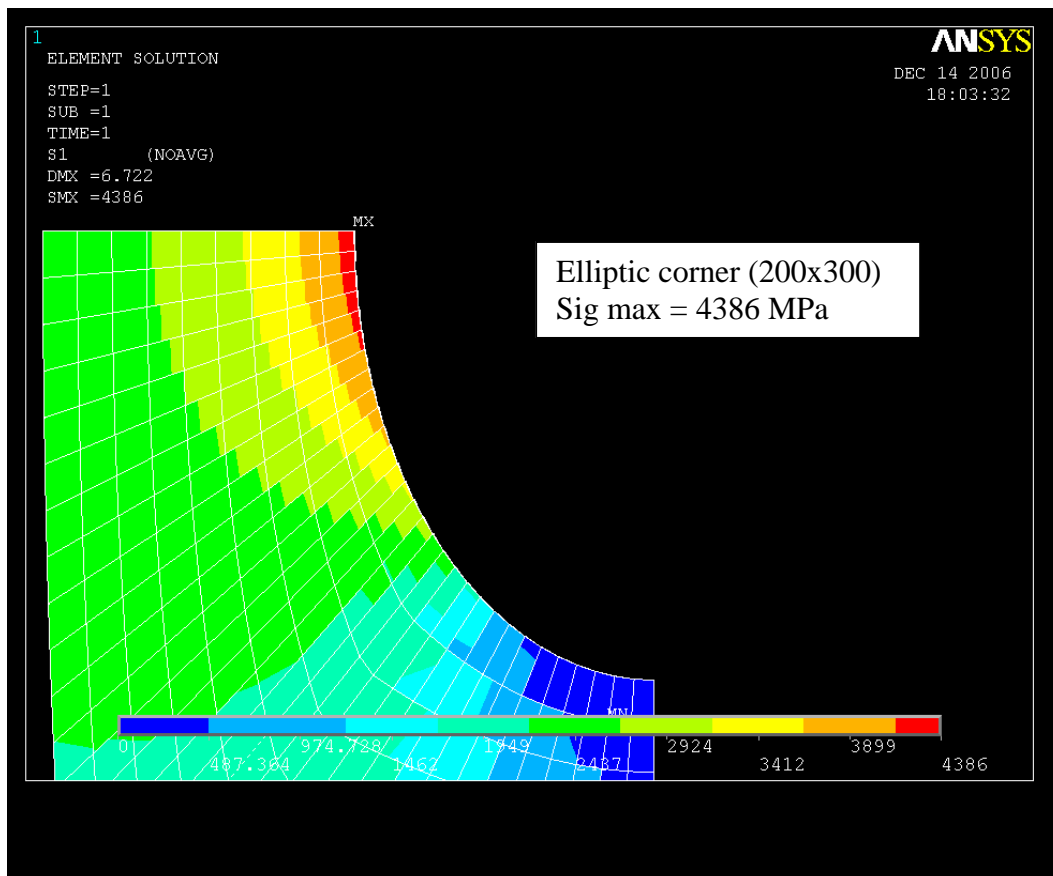
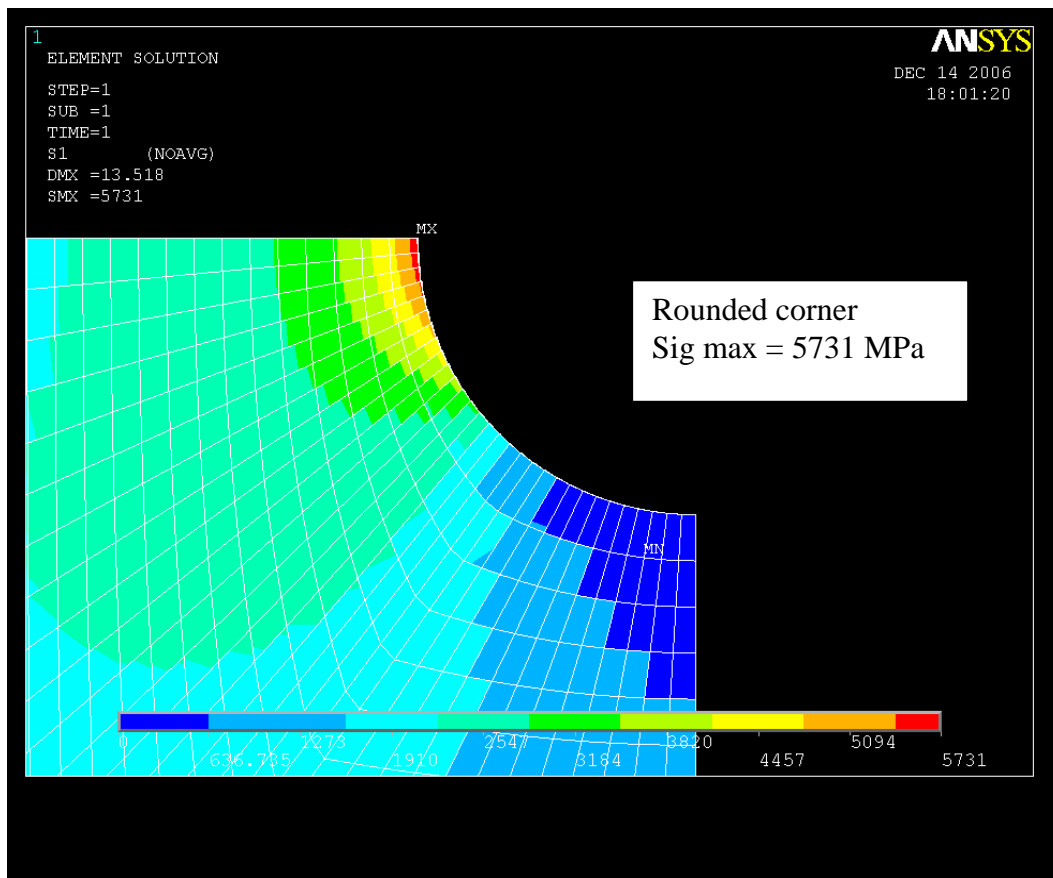
$$\varepsilon = 0.01$$

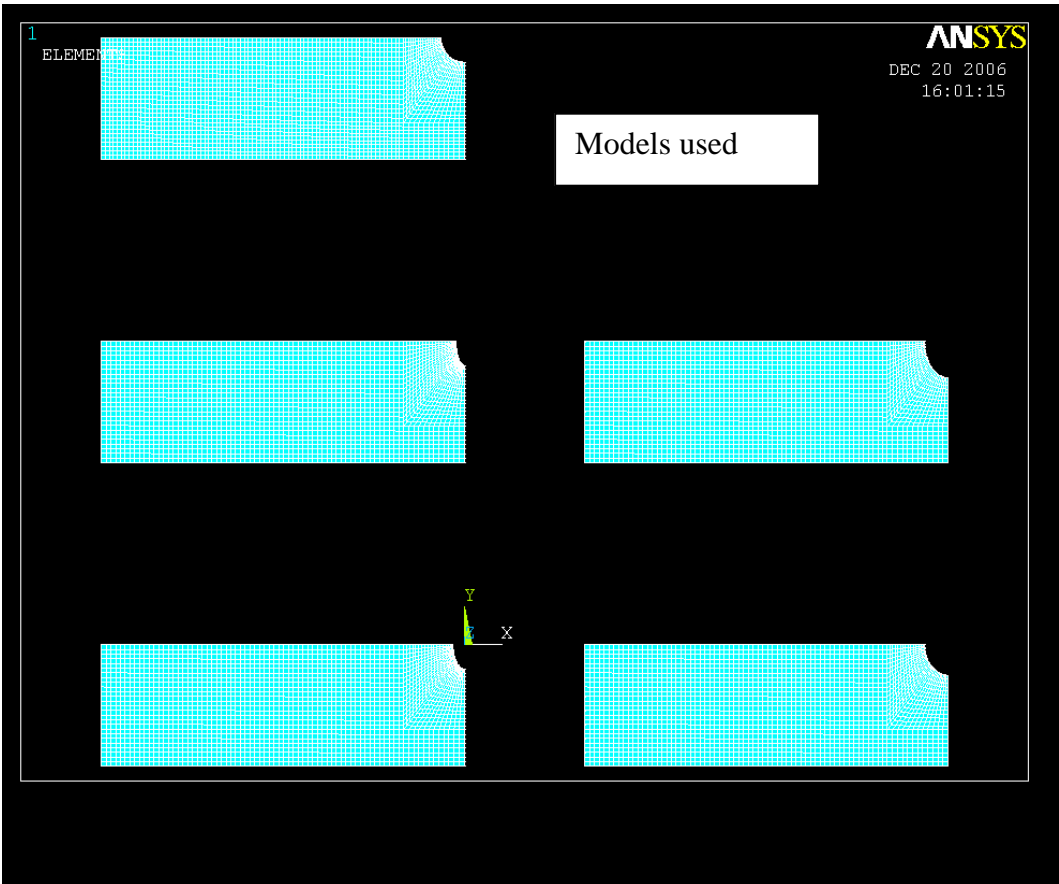
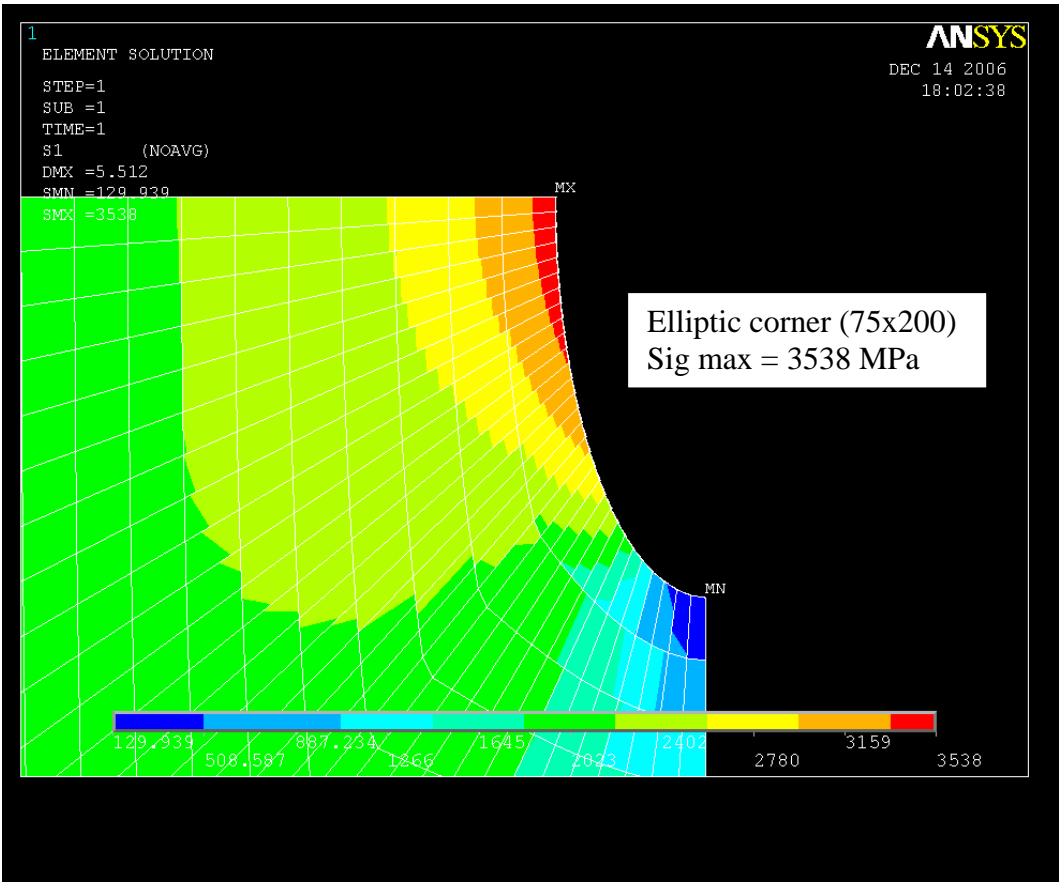
$$\sigma_{mean} = 2060 \text{ MPa}$$

- Maximum stress

This is the greatest principal stress read in the model as shown on the following pictures.

# ANSYS 9.0 tests





## Results

Comparison between  $K_t$  eval ( $f_c$ ) and  $K_t$  real (ANSYS software) for the different ellipses

Shape	dimensions	Maximum stress	$K_t$ real (Max stress/2060)	Correction factor $f_c$	$K_t$ evaluated ( $2.78 * f_c$ )	$K_t$ eval / $K_t$ real
Circular hole	200x200	5731	2.78	1		
Ellipse 1	50x200	3057	1.48	0.5	1.39	0.94
Ellipse 2	75x200	3538	1.72	0.58	1.62	0.94
Ellipse 3	100x200	4009	1.95	0.67	1.85	0.95
Ellipse 4	200x250	4928	2.39	0.87	2.42	1.01
Ellipse 5	200x300	4386	2.13	0.78	2.17	1.02
Ellipse 6	200x400	3702	1.8	0.67	1.85	1.03

We can see that  $r_b$  radius is a more conservative basis than  $r_a$  to evaluate the influence of an elliptic shape. The error is a bit less than for  $r_a$  and the  $K_t$  obtained is over evaluated ( $r_b$  basis) instead of being under evaluated ( $r_a$ ).

